

Slip Flow Model

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- ☐ Separated flow model requires a large number of closing relations.
- ☐ Many of these are difficult to be specified universally
- ☐ Simpler concepts to account for slip and empirically closing for slip is often practiced and is called slip flow model
- ☐ $p_l = p_g$ is invoked, implying mechanical equilibrium
- ☐ Better models have been tried for wall shear representation
- ☐ We shall look at these.

Mixture Mass Conservation

- We had derived the mass balance as

$$\frac{\partial \rho_m}{\partial t} + \frac{\partial \rho_m u_m}{\partial s} = 0 \quad (1)$$

- As derived earlier, the definitions of mixture quantities are given by

$$\rho_m = \rho_l(1 - \alpha) + \rho_g \alpha \quad \rho_m u_m = (\rho_l u_l(1 - \alpha) + \rho_g u_g \alpha) \quad (2)$$

- It may be noted that $\rho_m u_m = \frac{\dot{m}}{A} = G \quad (2)$

- ☐ The simplified momentum equation comes from the mixture momentum equation

$$\frac{\partial(\alpha \rho_g u_g + (1 - \alpha) \rho_l u_l)}{\partial t} + \frac{\partial(\alpha \rho_g u_g^2 + (1 - \alpha) \rho_l u_l^2)}{\partial s} = -\alpha \frac{\partial p_g}{\partial x}$$

$$-(1 - \alpha) \frac{\partial p_l}{\partial x} - \frac{\tau_{wg} s_g}{A} - \frac{\tau_{wl} s_l}{A} - (\alpha \rho_g + (1 - \alpha) \rho_l) g \sin \theta \quad (3)$$

- ☐ This can be written as

$$\frac{\partial \rho_m u_m}{\partial t} + \frac{\partial(\alpha \rho_g u_g^2 + (1 - \alpha) \rho_l u_l^2)}{\partial s} = -\frac{\partial p}{\partial x} - \frac{\tau_w P}{A} - \rho_m g \sin \theta \quad (4)$$

- ☐ The term, $\alpha \rho_g u_g^2 = \frac{\alpha \rho_g \dot{m}_g^2}{(A \alpha \rho_g)^2} = \frac{\dot{m}_g^2}{A^2} \frac{x^2}{\alpha \rho_g} \quad (5)$

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Momentum Equation-II

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□ Similarly, $(1-\alpha)\rho_l u_l^2 = \frac{\dot{m}^2 (1-x)^2}{A^2 (1-\alpha)\rho_l}$ 6

□ The second term can now be written as

$$\frac{\partial(\alpha\rho_g u_g^2 + (1-\alpha)\rho_l u_l^2)}{\partial s} = \frac{\partial}{\partial s} \left(\frac{\dot{m}^2}{A^2} \left(\frac{x^2}{\alpha\rho_g} + \frac{(1-x)^2}{(1-\alpha)\rho_l} \right) \right) = \frac{\partial}{\partial s} \left(\frac{\dot{m}^2}{A^2 \rho'} \right)$$

□ Where, $\left(\frac{x^2}{\alpha\rho_g} + \frac{(1-x)^2}{(1-\alpha)\rho_l} \right) = \frac{1}{\rho'}$ 7

Momentum
Density

□ Thus momentum equation can be written as

$$\frac{\partial \rho_m u_m}{\partial t} + \frac{\partial}{\partial s} \left(\frac{(\rho_m u_m)^2}{\rho'} \right) = -\frac{\partial p}{\partial x} - \frac{\tau_w P}{A} - \rho_m g \sin \theta$$
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Total Energy Equation-I

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□ Assuming shear and pressure work is negligible in the system and neglecting shaft work, we can write

$$\frac{\partial \left(\rho_g A_g \left(e_g - \frac{p}{\rho_g} \right) + \rho_l A_l \left(e_l - \frac{p}{\rho_l} \right) \right)}{\partial t} + \frac{\partial (\dot{m}_g e_g + \dot{m}_l e_l)}{\partial s} = \dot{q}$$

$$\frac{\partial (\rho_g \alpha e_g + \rho_l (1-\alpha) e_l)}{\partial t} + \frac{\partial (\dot{m}_g e_g + \dot{m}_l e_l)}{\partial s} = A \frac{\partial p}{\partial t} + \dot{q}$$

$$\Rightarrow \frac{\partial (\rho_g \alpha e_g + \rho_l (1-\alpha) e_l)}{\partial t} + \frac{\partial (\dot{m} (x e_g + (1-x) e_l))}{\partial s} = A \frac{\partial p}{\partial t} + \dot{q}$$

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Total Energy Equation-II

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• Defining $\rho_m e_m = (\rho_l e_l (1-\alpha) + \rho_g e_g \alpha)$ 9

$$\frac{\partial (\rho_m e_m)}{\partial t} + \frac{\partial (\dot{m} (x e_g + (1-x) e_l))}{\partial s} = \frac{\partial p}{\partial t} + \dot{q}$$

$$\Rightarrow \frac{\partial (\rho_m e_m)}{\partial t} + \frac{\partial (\dot{m} (x h_g + (1-x) h_l))}{\partial s} + \frac{\partial \left(\dot{m} \left(x \frac{u_g^2}{2} + (1-x) \frac{u_l^2}{2} + H \right) \right)}{\partial s} = A \frac{\partial p}{\partial t} + \dot{q}$$
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Summary

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$$\frac{\partial \rho_m}{\partial t} + \frac{\partial \rho_m u_m}{\partial s} = 0$$

$$\frac{\partial \rho_m u_m}{\partial t} + \frac{\partial}{\partial s} \left(\frac{(\rho_m u_m)^2}{\rho'} \right) = -\frac{\partial p}{\partial x} - \frac{\tau_w P}{A} - \rho_m g \sin \theta$$

$$\Rightarrow \frac{\partial (\rho_m e_m)}{\partial t} + \frac{\partial (\dot{m} (x h_g + (1-x) h_l))}{\partial s} + \frac{\partial \left(\dot{m} \left(x \frac{u_g^2}{2} + (1-x) \frac{u_l^2}{2} + H \right) \right)}{\partial s} = A \frac{\partial p}{\partial t} + \dot{q}$$

Variables $\dot{m}, x, \alpha, \rho_g, \rho_l, p, \tau_w, h_g, h_l, q'$ 10

Equations 3

Closing relations required 7

$$\rho_g = \rho_g(p) \quad 1 \quad \rho_l = \rho_l(p) \quad 1$$

$$h_g = h_g(p) \quad 1 \quad h_l = h_l(p) \quad 1$$

$$\text{model for } \tau_w \quad 1 \quad \text{model for } \alpha \text{ or for slip} \quad 1$$

$$q' \text{ Modelled or externally specified} \quad 1$$