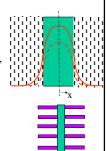
Extended Heat Transfer-I

- · Consider a slab fuel with volumetric heat generation. If it is cooled by an efficient media, then the temperature profile is as shown in the dotted line
- If the heat transfer coefficient is poor, then the fluid temperature drop will be more and the centerline temperature will also increase as shown by the dark line
- This will lead to unacceptably high temperature. One way of reducing the temperature would be by attaching fins to the outside surface



Extended Heat Transfer-II

Addition of fins reduce convective resistance by increasing A

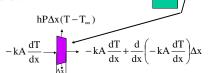
$$R_{conv} = \frac{1}{hA}$$



- · Heat transfer by addition of surface area is called extended heat transfer or fin heat transfer
- Heat transfer in Fin is by both convection and conduction
- Though strictly not one dimensional, it can be approximated by one dimensional heat transfer
- Since it is a model used for analysis, we shall derive the fin equation from basics

Governing equations for Fins-I

• In general, let the fin be of varying cross section as shown



• In steady state, heat in should be equal to heat out

$$-kA\frac{dT'}{dx} - \left[-kA\frac{dT'}{dx} + \frac{d}{dx} \left(-kA\frac{dT}{dx} \right) \Delta x \right] - hP\Delta x (T - T_{\infty}) = 0$$
In out out

Governing equations for Fins-II

$$\frac{d}{dx}\left(kA\frac{dT}{dx}\right) - hP(T - T_{\infty}) = 0$$

If k of the fin is constant, then,

$$\frac{d}{dx}\left(A\frac{dT}{dx}\right) - \frac{hP}{k}(T - T_{\infty}) = 0$$

• If the fin is prismatic, then, A is independent of x

$$\Rightarrow \frac{d^2T}{dx^2} - \frac{hP}{kA}(T - T_{\infty}) = 0$$

• Defining $(T-T_{\infty}) = \theta$, and $(hP/kA) = m^2$, we have

$$\Rightarrow \frac{\mathrm{d}^2 \theta}{\mathrm{d}x^2} - \mathrm{m}^2 \theta = 0$$

Governing equations for Fins-III

• The governing equation is a second order differential equation and its solution can be expressed as

$$\theta = C_1 e^{mx} + C_2 e^{-mx}$$

- The Boundary condition for the above equation is usually idealized conditions
- At the base of the fin, the temperature is usually specified as T_b

$$\Rightarrow \theta = \theta_{\rm h} = T_{\rm h} - T_{\infty} \text{ at } x = 0$$

• The commonly used boundary condition at the tip is what is known as insulated tip boundary

Governing equations for Fins-IV

· This is expressed as

$$\Rightarrow \frac{dT}{dx} = 0 \Rightarrow \frac{d\theta}{dx} = 0 \text{ at } x = L$$

• Boundary condition at x = 0, gives

$$\theta_b = C_1 + C_2$$

• Boundary condition at x = L, gives

$$0 = C_1 \dot{m} e^{mL} + C_2 (-\dot{m}) e^{-mL}$$

$$\Rightarrow 0 = C_1 e^{mL} - (\theta_b - C_1) e^{-mL}$$

$$\Rightarrow C_1 = \theta_b \frac{e^{-mL}}{mL}$$

$$\Rightarrow C_1 = \theta_b \frac{e^{-mL}}{e^{mL} + e^{-mL}} \qquad C_2 = \theta_b - C_1 = \theta_b - \theta_b \frac{e^{-mL}}{e^{mL} + e^{-mL}}$$

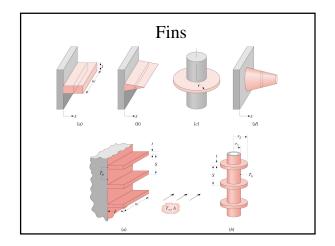
Governing equations for Fins-V

$$\Rightarrow C_2 = \theta_b \frac{e^{mL}}{e^{mL} + e^{-mL}}$$

$$\therefore \theta = \theta_b \frac{e^{-mL}e^{mx} + e^{mL}e^{-mx}}{e^{mL} + e^{-mL}}$$

$$= \theta_b \frac{e^{-m(L-x)} + e^{m(L-x)}}{e^{mL} + e^{-mL}}$$

$$\theta = \theta_b \frac{\cosh m(L-x)}{\cosh mL}$$



Fin Heat Transfer -I

 θ_{b}

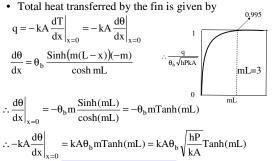
• We Studied the case of Fin with insulated tip and obtained the solution as

$$\theta = \theta_b \frac{\cosh m(L - x)}{\cosh mL}$$

- The parameter mL is non-dimensional and decides the character of the fin
- mL=1 is kind of under-designed fin and mL=5 will be a over designed fin with material waste, mL=3 is considered a good number for fin design
- Let us get more information by obtaining the total heat transfered

Fin Heat Transfer -II

• Total heat transferred by the fin is given by



Fin Heat Transfer -II

- · As the boundary conditions are modified, or variable area fins are concerned, the subject gets more complicated and will be left to specialists
- However, to help non-specialists use complex results and interpret them, some simple parameters are defined.
- The first one is fin effectiveness ε_f

$$\epsilon_{\rm f} = \frac{Heat \ transferred \ with \ fin}{Heat \ transferred \ without \ fin} = \frac{q_{with \ fin}}{q_{without \ fin}}$$

• For the case we have analysed

$$\epsilon_{\rm f} = \frac{\theta_b \sqrt{hPkA} Tanh(mL)}{\theta_b hA} = \sqrt{\frac{kP}{hA}} Tanh(mL)$$

Fin Heat Transfer -III

• Another measure used is the fin efficiency η_f

 \therefore q = $\theta_h \sqrt{hPkA}Tanh(mL)$

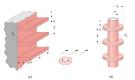
Heat transferred with fin Heat transferred with entire fin at base temperature

$$\eta_{\rm f} = \frac{\theta_{\rm b} \sqrt{hPkA} \, Tanh(mL)}{\theta_{\rm b} hPL} = \sqrt{\frac{kA}{hP}} \, \frac{Tanh(mL)}{L} = \frac{Tanh(mL)}{mL}$$

- The value of η_f is generally dependent on the non-dimensional parameter mL and expressions are available for complex geometries.
- The definitions of P and A have to be carefully understood. This you can do in the homework

Fin Heat Transfer -IV

 The real interest in engineering is not a single fin but a fin array such as the ones shown



- Let us now define the following areas
- A_{uf} is the total area that is not finned (unfinned)
- A_f is the each fin surface area (perimeter x Length)
- Heat transferred by the fins can be given by

$$q_f = \text{NhPL}\theta_b\eta_f = \text{NhA}_f\theta_b\eta_f$$

Fin Heat Transfer -V

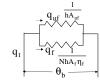
• Heat transferred by the unfinned area

$$q_{uf} = hA_{uf}\theta_b$$

• Total Heat transferred

$$q_t = q_f + q_{uf} = NhA_f\theta_b\eta_f + hA_{uf}\theta_b$$

• In terms of electrical analogy



Fin Heat Transfer -VI

- Many times the fins are not metallurgically bonded but shrink fitted or bonded with adhesives
- This adds contact resistance
- This can easily be accommodated using electrical analogy

