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Computational Methods in Thermal and Fluids Engineering

Solution of Elliptic Equations

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- One of the most common elliptic equation is the Steady Heat Equation

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} = -\frac{q'''}{k}$$

- Fully developed 2-D incompressible flow in ducts can be reduced to an elliptic equation as follows

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \Rightarrow v = 0 \text{ everywhere}$$

$$\left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \frac{\mu}{\rho} \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right] \Rightarrow \frac{\partial p}{\partial x} = \mu \frac{\partial^2 u}{\partial y^2}$$

$$\left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \frac{\mu}{\rho} \left[\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right] \Rightarrow \frac{\partial p}{\partial y} = 0 \Rightarrow p = p(x)$$

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$$\frac{\partial p}{\partial x} = \mu \frac{\partial^2 u}{\partial y^2} \Rightarrow \frac{\partial^2 u}{\partial y^2} = \frac{1}{\mu} \frac{\partial p}{\partial x} = C$$

f(x) **f(y)**

- A similar extension to 3-D with v=0 and w=0 leads to

$$\frac{\partial p}{\partial x} = \mu \left[\frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial w^2} \right]$$

- In general, the above can be summed into

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0 \quad \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = f(x, y)$$

Laplace Eq. **Poisson Eq.**

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- Comparing with our standard form

$$A f_{xx} + B f_{xy} + C f_{yy} + D f_x + E f_y + F = 0$$

B = 0

- For positive A and C, $B^2 - 4AC < 0$
- The equations are elliptic
 - No characteristic directions
 - No discontinuities
 - Information spreads in all directions
 - Every point affects every other point

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Jacobi and Gauss Siedel

- ❑ Jacobi (for S = 0)

$$T_{i,j}^{k+1} = \frac{T_{i+1,j}^k + T_{i-1,j}^k + (T_{i,j+1}^k + T_{i,j-1}^k)\beta^2}{2(1 + \beta^2)}$$

- ❑ Assume T⁰ and iterate using the above relation
- ❑ If the new values available are immediately used for other points, it is called Gauss Siedel

$$T_{i,j}^{k+1} = \frac{T_{i+1,j}^k + T_{i-1,j}^{k+1} + (T_{i,j+1}^k + T_{i,j-1}^{k+1})\beta^2}{2(1 + \beta^2)}$$

- ❑ The necessary and sufficient condition for convergence is the Scarborough Criterion (Diagonal ≥ sum of off-diagonal and Diagonal > sum of off-diagonal at least in one row)

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Line Method

- ❑ In point method, information flows from point to point
- ❑ Hence, the information from one boundary to another takes more time and it takes more effort to get convergence
- ❑ If we can facilitate exchange of information quickly, we can converge faster
- ❑ Line methods accomplish this effectively

$$T_{i-1,j}^{k+1} - 2(1 + \beta^2)T_{i,j}^{k+1} + T_{i+1,j}^{k+1} = -\beta^2(T_{i,j-1}^{k+1} + T_{i,j+1}^k)$$

- ❑ The idea is to construct the Tri-diagonal matrix and solve them by TDMA

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ADI Method

- ❑ In line by line the information from one set of boundaries moves fast but not from the other
- ❑ This can be accelerated, if we can alternate the direction
- ❑ This method is called Alternate Direction Implicit
- ❑ The iteration cycle has two parts.

X-Sweep

$$T_{i-1,j}^{k+0.5} - 2(1 + \beta^2)T_{i,j}^{k+0.5} + T_{i+1,j}^{k+0.5} = -\beta^2(T_{i,j-1}^{k+0.5} + T_{i,j+1}^k)$$

Y-Sweep

$$\beta^2 T_{i,j-1}^{k+1} - 2(1 + \beta^2)T_{i,j}^{k+1} + \beta^2 T_{i,j+1}^{k+1} = -T_{i+1,j}^{k+0.5} - T_{i-1,j}^{k+1}$$

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Acceleration Procedures-I

- ❑ Point-SOR
- ❑ The essence is that for a linear system it has been seen that we can accelerate by over relaxation

$$T_{i,j}^{k+1} = \alpha T_{i,j}^{k+1}|_{GS} + (1 - \alpha)T_{i,j}^k$$

- ❑ The value of this over relaxation parameter, α, is > 1
- ❑ Substituting and rearranging gives

$$T_{i,j}^{k+1} = T_{i,j}^k + \alpha (T_{i,j}^{k+1}|_{GS} - T_{i,j}^k)$$

$$T_{i,j}^{k+1} = T_{i,j}^k + \frac{\alpha}{2(1 + \beta^2)} (T_{i+1,j}^k + T_{i-1,j}^{k+1} + (T_{i,j+1}^k + T_{i,j-1}^{k+1})\beta^2 - 2(1 + \beta^2)T_{i,j}^k)$$

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Acceleration Procedures-II

- ❑ Line-SOR
 - ❑ The equation derived in the previous equation can be rearranged as

Same Eq.

$$T_{i,j}^{k+1} = T_{i,j}^k + \frac{\alpha}{2(1+\beta^2)} (T_{i+1,j}^k + T_{i-1,j}^{k+1} + (T_{i,j+1}^k + T_{i,j-1}^{k+1})\beta^2 - 2(1+\beta^2)T_{i,j}^k)$$

$$2(1+\beta^2)T_{i,j}^{k+1} = 2(1+\beta^2)T_{i,j}^k + \alpha(T_{i+1,j}^k + T_{i-1,j}^{k+1} + (T_{i,j+1}^k + T_{i,j-1}^{k+1})\beta^2 - 2(1+\beta^2)T_{i,j}^k)$$

$$\alpha T_{i+1,j}^{k+1} - 2(1+\beta^2)T_{i,j}^{k+1} + \alpha T_{i-1,j}^{k+1} = -(1-\alpha)2(1+\beta^2)T_{i,j}^k - \alpha(T_{i,j+1}^k + T_{i,j-1}^k)\beta^2$$

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Acceleration Procedures-III

- ❑ Accelerated ADI
 - ❑ The equation derived for LSOR can be rearranged as

X-Sweep

$$\alpha T_{i+1,j}^{k+0.5} - 2(1+\beta^2)T_{i,j}^{k+0.5} + \alpha T_{i-1,j}^{k+0.5} = -(1-\alpha)2(1+\beta^2)T_{i,j}^k - \alpha(T_{i,j+1}^k + T_{i,j-1}^k)\beta^2$$

Y-Sweep

$$\alpha\beta^2 T_{i,j+1}^{k+1} - 2(1+\beta^2)T_{i,j}^{k+1} + \alpha\beta^2 T_{i,j-1}^{k+1} = -(1-\alpha)2(1+\beta^2)T_{i,j}^{k+0.5} - \alpha(T_{i+1,j}^{k+0.5} + T_{i-1,j}^{k+1})$$

- ❑ Relative Comparison
 - ❑ For a 21X41 nodes for a slab of 1X2 with one of the smaller side held at 1, and for the same accuracy, results have been given in Hoffman and Chiang
 - ❑ It is reproduced in next slide

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Acceleration Procedures-IV

Relative Comparison

Method	Iterations	Time (CPU)	α_{opt}
GS (point)	574	5.524	
GS(Line)	308	7.196	
PSOR	52	1.082	1.78
LSOR	36	1.410	1.265
ADI	157	6.693	
AADI	23	1.535	1.27