## PhD Qualifying Exam - July 2022

Manufacturing Processes-II
Maximum marks: 100
Time : 3 hours

- This is an Open Book, Open Notes and No internet Examination. You are expected to follow the instructions provided to you meticulously and submit your answer book accordingly.
- Answer any 5 questions. Each question carries 20 marks
- Make suitable assumptions, if required and mention them.

1. During deformation of material in machining, the shear strain, $(\gamma)$ is a function of shear angle, $(\varnothing)$ and rake angle, $(\alpha)$.
a. Derive the expression for shear strain in orthogonal machining.
b. Find the expression for shear angle as a function of ( $\alpha$ ) for the minimum shear strain condition.
c. Prove that the expression for chip ratio, $r$, as a function of $(\alpha)$ for minimum shear strain condition is:
[5 Marks]

$$
r=\frac{\sin \left(\frac{\pi}{4}+\frac{\alpha}{2}\right)}{\cos \left(\frac{\pi}{4}-\frac{\alpha}{2}\right)}
$$

2. This question contains two parts: 2 a and 2 b . Both parts are independent of each other.
a. For the orthogonal cutting of a particular work material, $\mu$ is the coefficient of friction at toolchip interface and $r$ is the cutting ratio. Assume that rake angle is zero. Show that the ratio of material shear strength $\left(\tau_{s}\right)$ to the specific cutting energy ( u ) is given by: Marks]

$$
\frac{\tau_{s}}{u}=\frac{(1-\mu r) r}{1+r^{2}}
$$

b. Surface roughness of the machined cylindrical surface was measured using a line profilometer (see Fig 1). The raw data of the surface heights collected by the profilometer is given in the table below. The X -axis direction is along the direction of travel of the profilometer and Z-axis is normal to surface.
Based on the data, find
i. If there is any form error in the raw measurement data. Justify your answer. [2 Marks]
ii. Find arithmetic mean roughness ( Ra ) of the surface. [4 Marks]
iii. Find surface straightness. [2 Marks]
iv. Comment on an estimate of cylindricity of the machined component. [2 Marks] Show all the steps and state assumptions, if any.


Figure 1 : Question 2b
3. This question contains two parts: 3 a and 3 b . Both parts are independent of each other.
a. Design the general type of GO and NOT GO gauges for a 40 mm shaft and hole pair designated as $40 \mathrm{D} 8 / \mathrm{h} 9$, given that:
[15 Marks]
$i=0.453 D^{1 / 3}+0.001 D$
40 mm lies in the diameter range of $30-50 \mathrm{~mm}$
$\mathrm{IT} 8=25 i \quad$ and $\quad \mathrm{IT9}=40 i$
Upper and lower deviations for shafts are given in the table below
Gauge tolerance $=10 \%$ of work tolerance
Wear allowance $=10 \%$ of gauge tolerance

| Upper deviation (es) |  | Lower deviation (ei) |  |
| :---: | :---: | :---: | :---: |
| Shaft designation | In $\mu \mathrm{m}$ ( for $D$ in mm ) | Shaft designation | In $\mu \mathrm{m}$ (for $D$ in mm ) |
| SHAFTS | $=-(265+1.3 D)$ for $D \leq 120$ | j5-j8 | No formula |
|  |  | (For js two deviations are equal to IT $\pm 2$ ) |  |
| a | $=-3.5 D$ for $D>120$ | k4-k7 | $=+0.6 \sqrt[3]{D}$ |
|  |  | For grades $\leq k 3$ to $\geq \mathrm{k} 8$ | $=0$ |
| b | $=-(140+0.85 D)$ for $D \leq 160$ | m | $=+$ (IT7 - IT6) |
|  | $\begin{aligned} & =-1.8 D \\ & \text { for } D>160 \end{aligned}$ | n | $=+5 D^{0.34}$ |
|  |  | P | $=+177+0$ to 5 |
| C | $=-52 D^{02}$ for $D+177+0$ to 40 | r | $=$ Geometric mean of ei values for $p$ and $s$ |
|  | $=-(95+0.8 D)$ for $D>40$ |  | $=+1 T 8+1$ to 4 for $D \leq 50$ |
| d | $=-16 D^{0.4}$ | s | $=+1 \mathrm{~T} 7+0.4 \mathrm{D}$ for $D>50$ |
| e | $=-11 D^{0.41}$ | t | $=+1 T 7+0.63 \mathrm{D}$ |
| $f$ | $=-5.5 D^{0.41}$ | u | $=+1 T 7+D$ |
| 9 | $=-2.5 D^{0.34}$ | $v$ x | $\begin{aligned} & =+\mid T 7+1.25 D \\ & =+\mid T 7+1.6 D \end{aligned}$ |
|  |  | y | $=+1 T 7+2 D$ |
| h | $=0$ | z | $=+1 \mathrm{~T}^{+}+2.5 \mathrm{D}$ |
|  |  | za | $=+1 T 8+3.15 \mathrm{D}$ |
|  |  | zb | $=+1 T 9+4 \mathrm{D}$ |
|  |  | ZC | $=+1 T 10+5 D$ |

b. In deep hole drilling of metals using electrochemical machining, what kind of electrolytes are preferred? Provide an explaination.
[5 Marks]
4. A manufacturing plant produces certain parts by drilling a through hole of diameter $D$ at the center of aluminium blocks having a geometry of a cube with an edge length $l$. The process is carried out at a constant rotational speed of the drill equal to $N$. Identical drill bits of semi point angle $\theta$ and diameter $D$ are used at varying feed rates $f(\mathrm{~m} /$ rotation). The cost of a drill bit is $R$, and the labor and overhead charges are $L$ and $B$ per hour, respectively. Once a tool is worn out, it is replaced with a new one. The tool changing time is $\mathrm{t}_{\mathrm{c}}$. The relationship between the tool life $t$ (in minutes) and the cutting parameters is given by the generalised Taylor's equation $\mathrm{vt}^{\mathrm{n}} \mathrm{a}^{\mathrm{p}} \mathrm{w}^{\mathrm{q}}=$ C, where $v(\mathrm{~m} / \mathrm{min})$ is the cutting speed, $a$ is the uncut chip thickness and $w$ is the width of cut. Both $a$ and $w$ are expressed in meters, and $C$ is a constant. Derive an expression for the optimal feed rate $(f)$ for maximum productivity. Assume any missing information and clearly outline the assumptions (if any).
[20 Marks]
5. In an ultrasonic finishing operation, a 20 mm diameter titanium tool is used to finish a copper plate. The tool vibrates with a frequency of 20 kHz , at an amplitude of $40 \mu \mathrm{~m}$ (from mean position). An abrasive slurry containing $5 \mu \mathrm{~m} \mathrm{SiC}$ particles at a concentration of $40 \%$ by volume is used. When the mean gap between the tool and workpiece is $50 \mu \mathrm{~m}$, it was observed that the indentation per particle is 1 nm and the etch rate of the surface is $10 \mathrm{~nm} / \mathrm{s}$. The impact efficiency is observed to be a function of the minimum tool workpiece gap ( $\mathrm{h}_{\min }$ ), given by $\beta=$
$\exp \left(\left(\mathrm{d}-\mathrm{h}_{\min }\right) / 10 \mathrm{~d}\right)$, where $d$ is the particle diameter. Calculate the etch rate of the surface in ( $\mathrm{nm} / \mathrm{s}$ ) if the mean gap is increased to $60 \mu \mathrm{~m}$.
[20 Marks]

## Given:

Density— $\mathrm{SiC}=3.21 \mathrm{~g} / \mathrm{cc}, \mathrm{Cu}=8.96 \mathrm{~g} / \mathrm{cc}, \mathrm{Ti}=4.5 \mathrm{~g} / \mathrm{cc}$,
Flow Stress - $\mathrm{Cu}=100 \mathrm{MPa}, \mathrm{Ti}=450 \mathrm{MPa}$
Hint: Use the grain throwing model of ultrasonic machining
6. This question contains two parts: $6 a$ and $6 b$. Both parts are independent of each other.
a. Consider a system where certain external events occur at random time intervals (i.e. the time-between-occurrence of these events is a random variable). Let there be two such external events namely E1 and E2, with their time-between-occurrence having Exponential probability density functions as $f_{1}(t)$ and $f_{2}(t)$ respectively. The mean time-between-occurrence for E1 and E2 can be taken as 100 hr and 50 hr respectively.
Occurrence of E1 can further trigger two events E3 and E4 with a probability of 0.5 and 0.3 respectively. Occurrence of E2 can further trigger two events E5 and E6 with a of 0.8 (i.e. $\mathrm{P}[\mathrm{E} 5 \mid \mathrm{E} 2]=\mathrm{P}[\mathrm{E} 6 \mid \mathrm{E} 2]=0.8$ ) provided E3 or E4 has occurred less than 100 hr before. However, if E 3 and E 4 have not occurred less than 100 hr before, then the probability values for occurrence of E5 and E6 given that E2 has occurred are 0.3 (i.e. $\mathrm{P}[\mathrm{E} 5 \mid \mathrm{E} 2]=\mathrm{P}[\mathrm{E} 6 \mid \mathrm{E} 2]=0.3$ ).
Explain in brief the theory and procedure (with an example and a schematic) behind random number generation using the inverse transform method and write the procedure for Simulating the occurrence of E3, E4, E5 and E6 for a given time period and demonstrate the method for a single simulation run for a 1000 hr interval and calculate the occurrence rates of E3, E4, E5 and E6.
[10 marks]
b. A process produces units in batches of size 100 . Consider an acceptance sampling plan which takes a random sample of size 10 from each batch and if more than 1 defective unit is found in the sample, the entire batch of 100 units will be rejected. Assume that the process producing these units has a defect rate of $10 \%$ (i.e. probability of a unit being defective is 0.1 ) when it is in an 'in-control' state. However, the inspection process used to check the sample is not perfect and has a 0.90 probability of detecting a defective unit (probability of declaring a good unit as defective can be assumed to be zero). At a random instance the process enters an 'out-of-control' state and starts producing $20 \%$ defective units.
Explain in detail the procedure for simulating the outcome of a sequence of batches to demonstrate the type 1 (wrongly rejecting a batch from an in-control process) and type 2 error (wrongly accepting a batch from an out-of-control process) for the sampling plan. Demonstrate the method for one batch each from 'in-control' and 'out-of-control' states.
[10 marks]
7. Consider a $n \times n$ chessboard. The knight is a piece in the game of chess, representing a knight (armored cavalry). The knight move is unusual among chess pieces. When it moves, it can move to a square that is two squares horizontally and one square vertically, or two squares vertically and one square horizontally. The complete move therefore looks like the letter $L$.
Knight's tour problem involves starting from a given square on a $n \times n$ chessboard and traversing the entire chessboard in $n^{2}$ moves such that the knight visits every square exactly once and returns to it's original starting position. A knight's tour is given in the following for an $8 \times 8$ chessboard.

Formulate the Knight's Tour problem on an $n \mathrm{n}$ chessboard as a linear (integer) program.
[20 Marks]


Figure Q7: Knight's tour in $8 \times 8$ chess board

